

Saddle-point masses in the Yukawa + LSD approach

J. Bartel

IPHC and Université Louis Pasteur, Strasbourg,

A. Dobrowolski

CEA-DAM, Bruyères-le-Châtel,

K. Pomorski

Uniwersytet M. C. Skłodowskiej, Lublin

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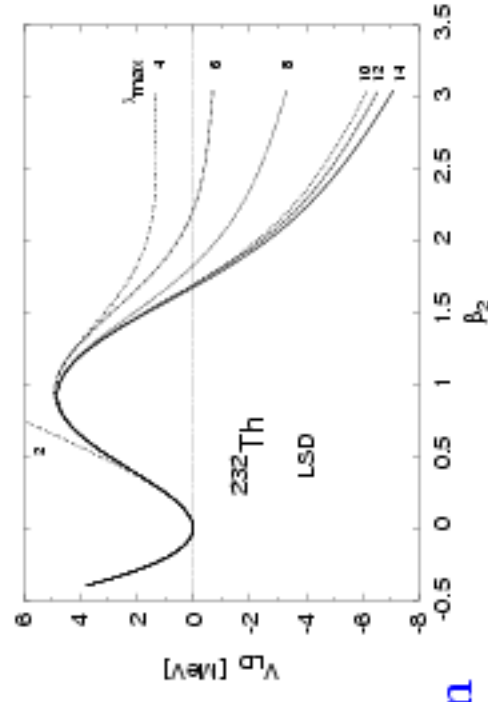


The ingredients

- Shape parametrisations for fissioning nuclei
- Macroscopic-Microscopic Model
- Fission barriers with different proton-neutron deformations
 - ▷ Stiffness of $E_{\text{mac}} \leftrightarrow$ shell + pairing effects
- Fission barriers with left-right asymmetry and non-axiality
- Conclusions

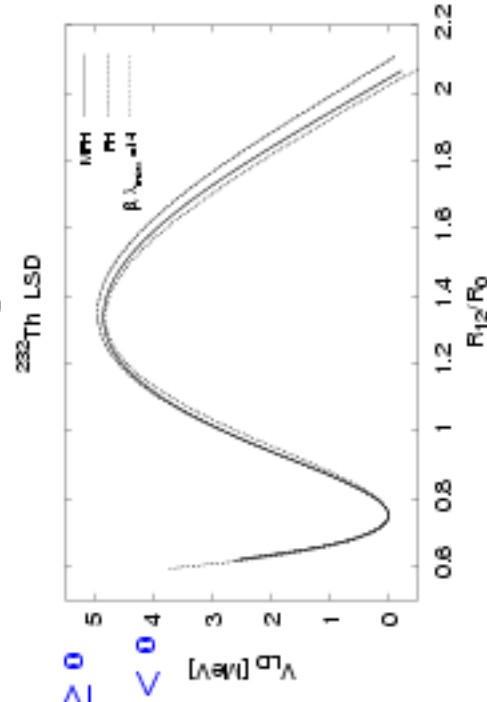
Shape parametrisations for fissioning nuclei

- Huge variety of nuclear shapes (g.s. \implies scission point)
- Only a very few relevant deformation parameters
 - Expansion in spherical harmonics



- Funny-Hills (FH) parametrisation

$$e_s^2(u) = \begin{cases} R_0^2 c^2 (1-u^2) (A + \alpha u + B u^2) & , B \geq 0 \\ R_0^2 c^2 (1-u^2) (A + \alpha u) \exp(B c^3 u^2) & , B < 0 \end{cases}$$

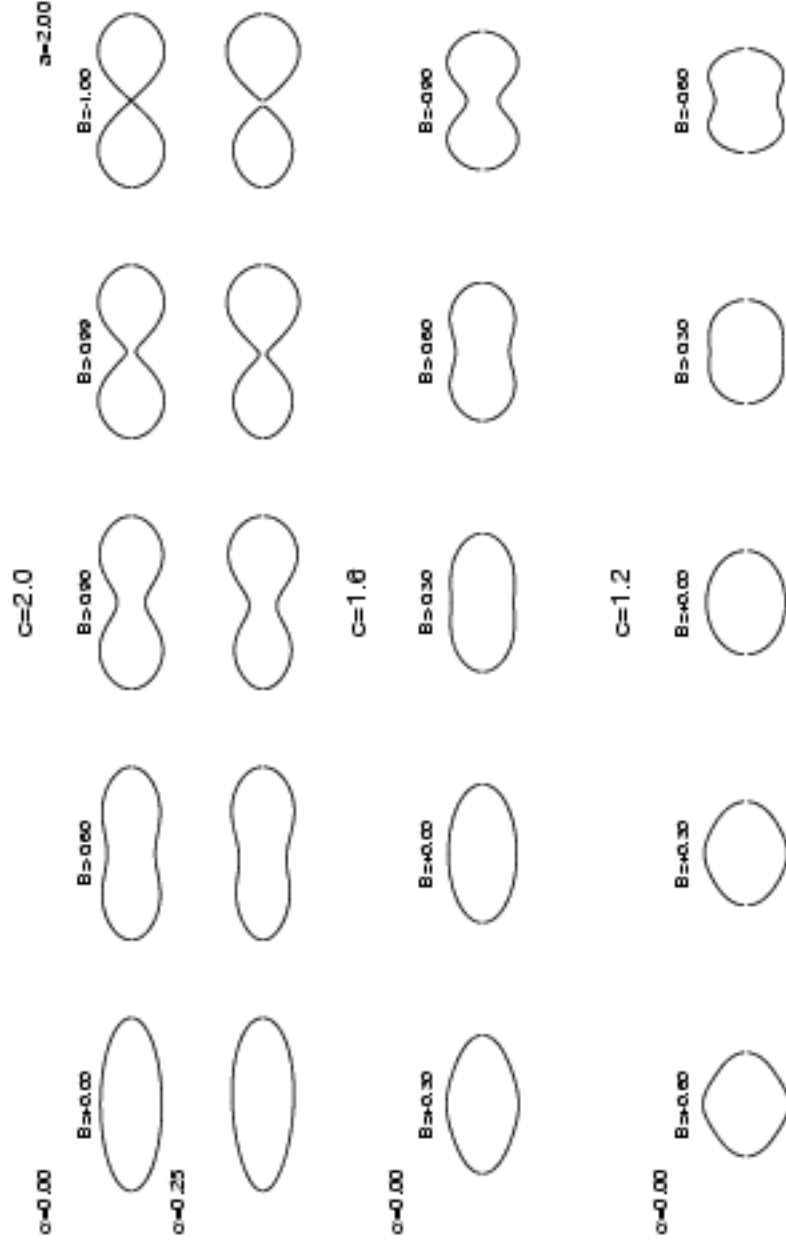


- Modified Funny-Hills shape parametrisation

$$\varrho_s^2(z) = \frac{R_o^2}{c f(a, B)} (1 - u^2) (1 + \alpha u - B e^{-a^2 u^2}),$$

where

$$f(a, B) = 1 - \frac{3B}{4a^2} \left[e^{-a^2} + \sqrt{\pi} \left(a - \frac{1}{2a} \right) \text{Erf}(a) \right]$$



breaking axial symmetry

suppose ellipsoidal shape \perp to z axis

and introduce the non-axiality parameter

$$\eta = \frac{a_y^2 - a_x^2}{a_y^2 + a_x^2}$$

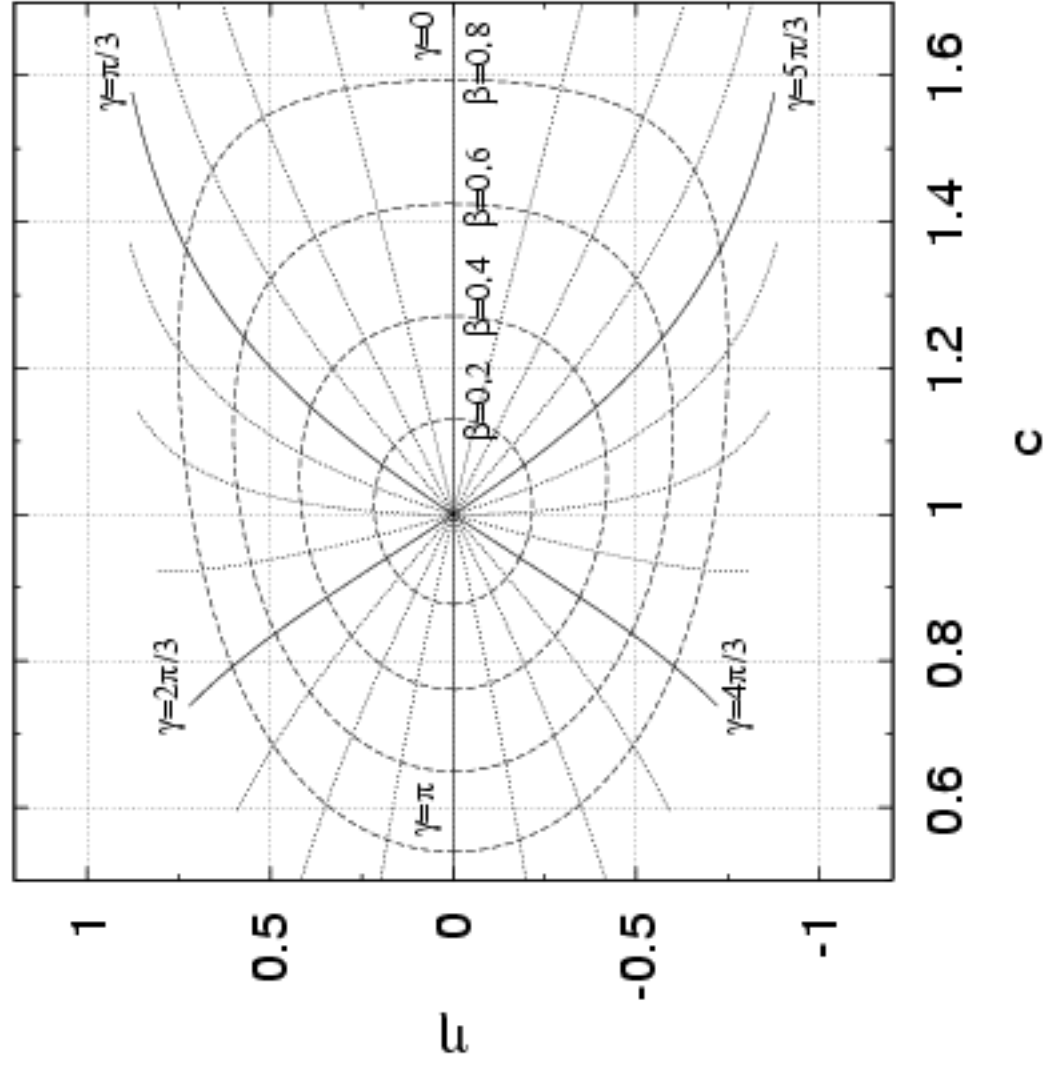
assume that η is independent of z

$$a_x(z) = \varrho_s(z) \left(\frac{1-\eta}{1+\eta} \right)^{1/4}$$

$$a_y(z) = \varrho_s(z) \left(\frac{1+\eta}{1-\eta} \right)^{1/4}$$

volume conservation then leads to

$$\tilde{\varrho}_s^2(z, \varphi) = \varrho_s^2(z) \frac{\sqrt{1-\eta^2}}{1+\eta \cos(2\varphi)}$$



Transformation from (c, η) to (β, γ) in the pure ellipsoidal case

Macroscopic-Microscopic Model

According to the Strutinski theorem

$$E_{\text{tot}} = \int \mathcal{H}(\rho) d^3r = E_{\text{mac}} + \delta E_{\text{mic}}$$

with Lublin-Strasbourg-Drop (LSD)

$$\begin{aligned} E_{\text{mac}}(Z, N, def) = & a_{\text{vol}}(1 - \kappa_{\text{vol}}I^2)A + a_{\text{surf}}(1 - \kappa_{\text{surf}}I^2)A^{2/3}B_{\text{surf}}(def) \\ & + a_{\text{cur}}(1 - \kappa_{\text{cur}}I^2)A^{1/3}B_{\text{cur}}(def) + \frac{3e^2}{5r_0} \frac{Z^2}{A^{1/3}} B_{\text{Coul}}(def) \\ & - C_4 \frac{Z^2}{A} - E_{\text{cong}} \end{aligned}$$

with shell and pairing corrections

$$\delta E_{\text{shell}} = \sum_{\text{occ}} \epsilon_\nu - \tilde{E}$$

$$\delta E_{\text{mic}} = \delta E_{\text{shell}} + \delta E_{\text{pair}}$$

$$\delta E_{\text{pair}} = E_{\text{BCS}} - \sum_{\text{occ}} \epsilon_\nu - \langle E_{\text{pair}} \rangle$$

Yukawa folded mean-field potentials

$$V_{\text{cen}}(\vec{r}) = \frac{V_o}{\rho_o} \int \rho(\vec{r}') g_\lambda(\vec{r}, \vec{r}') d^3 r' \quad \text{with} \quad \rho(\vec{r}) = \int \rho_{\text{sh}}(\vec{r}') g_a(\vec{r}, \vec{r}') d^3 r'$$

where

$$g_\lambda(\vec{r}, \vec{r}') = \frac{1}{4\pi\lambda^2} \frac{e^{-|\vec{r}-\vec{r}'|/\lambda}}{|\vec{r}-\vec{r}'|}$$

spin-orbit potential

$$V_{\text{s.o.}} = i \Lambda \vec{\nabla} V_{\text{cen}} \cdot [\vec{\sigma} \times \vec{\nabla}]$$

Parameters:

$$V_o^{(p)} = V_s + V_a \bar{\delta} \quad \text{and} \quad V_o^{(n)} = V_s - V_a \bar{\delta}$$

$$\bar{\delta} = \frac{I + D_1 Z^2 / A^{5/3}}{1 + D_2 / A^{1/3}}, \quad I = \frac{N - Z}{A}$$

$$\Lambda^{(p)} = C_{1p} A + C_{2p} \quad \text{and} \quad \Lambda^{(n)} = C_{1n} A + C_{2n}$$

Constants used in the Yukawa-folding procedure

constant	value	unit	constant	value	unit
λ	0.8	[<i>fm</i>]	a	0.7	[<i>fm</i>]
V_s	52.5	[<i>MeV</i>]	V_a	48.7	[<i>MeV</i>]
C_{1p}	$2.76 \cdot 10^{-4}$	[<i>MeV</i>]	C_{2p}	0.3092	[<i>MeV</i>]
C_{1n}	$2.07 \cdot 10^{-4}$	[<i>MeV</i>]	C_{2n}	0.3479	[<i>MeV</i>]
D_1	$1.1117 \cdot 10^{-2}$		D_2	3.15	

Fission barriers with different proton-neutron deformations

Potential energy through Yukawa folding

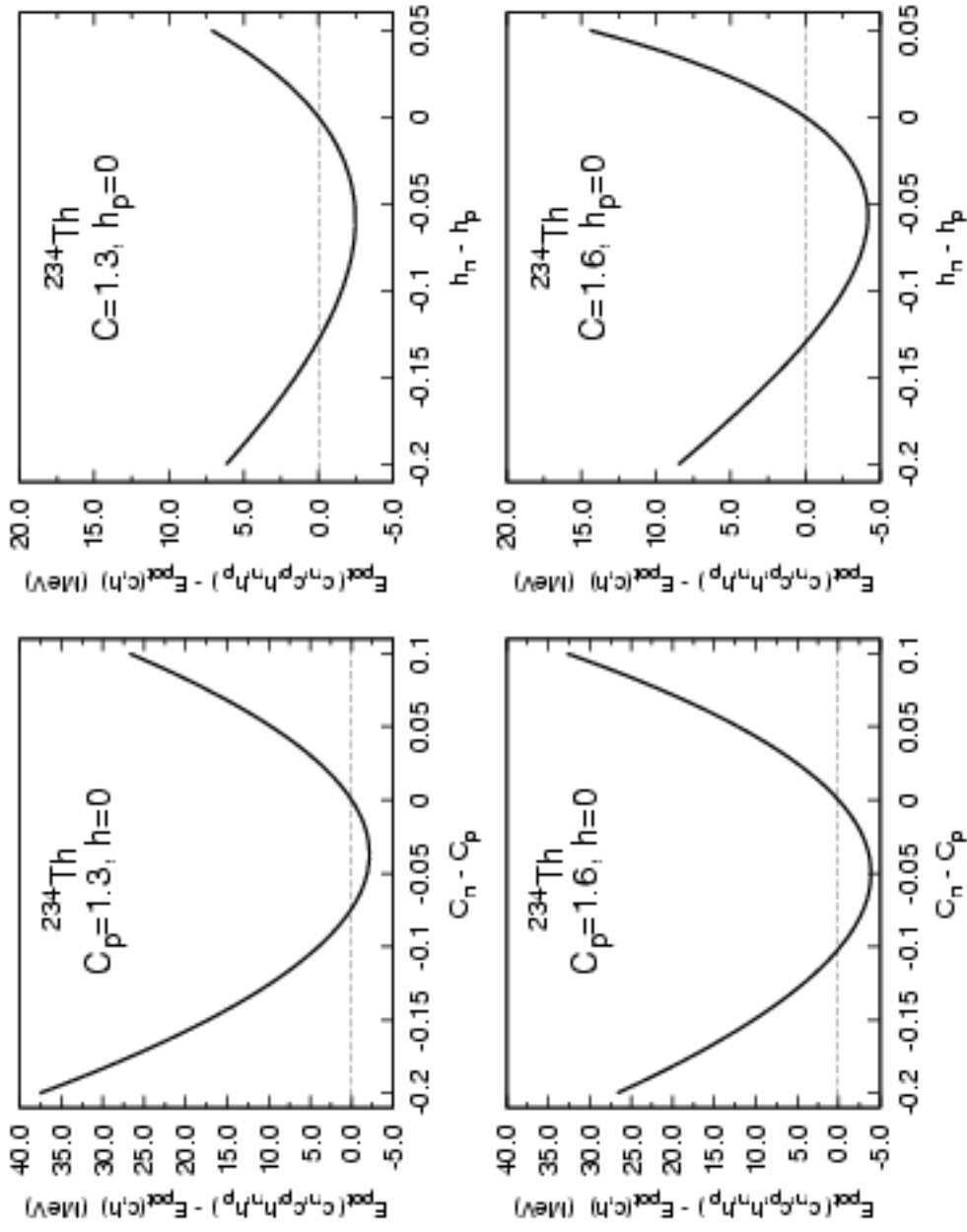
$$E_{\text{pot}} = \frac{V_0}{2a^3 \rho_0^2} \iint \rho(\vec{r}) g_\lambda(\vec{r}, \vec{r}') \rho(\vec{r}') d^3 r d^3 r'$$
$$\rho(\vec{r}) = \rho_n(\vec{r}) + \rho_p(\vec{r})$$

$$E_{\text{pot}}(\text{def}_p, \text{def}_n) = E_{pp} + E_{nn} + 2E_{pn}$$

where

$$E_{qq'} = \frac{V_0}{2a^3 \rho_0^2} \int_{V_q} \int_{V_{q'}} g_\lambda(\vec{r}, \vec{r}') \rho_q(\vec{r}) \rho_{q'}(\vec{r}') d^3 r d^3 r'$$

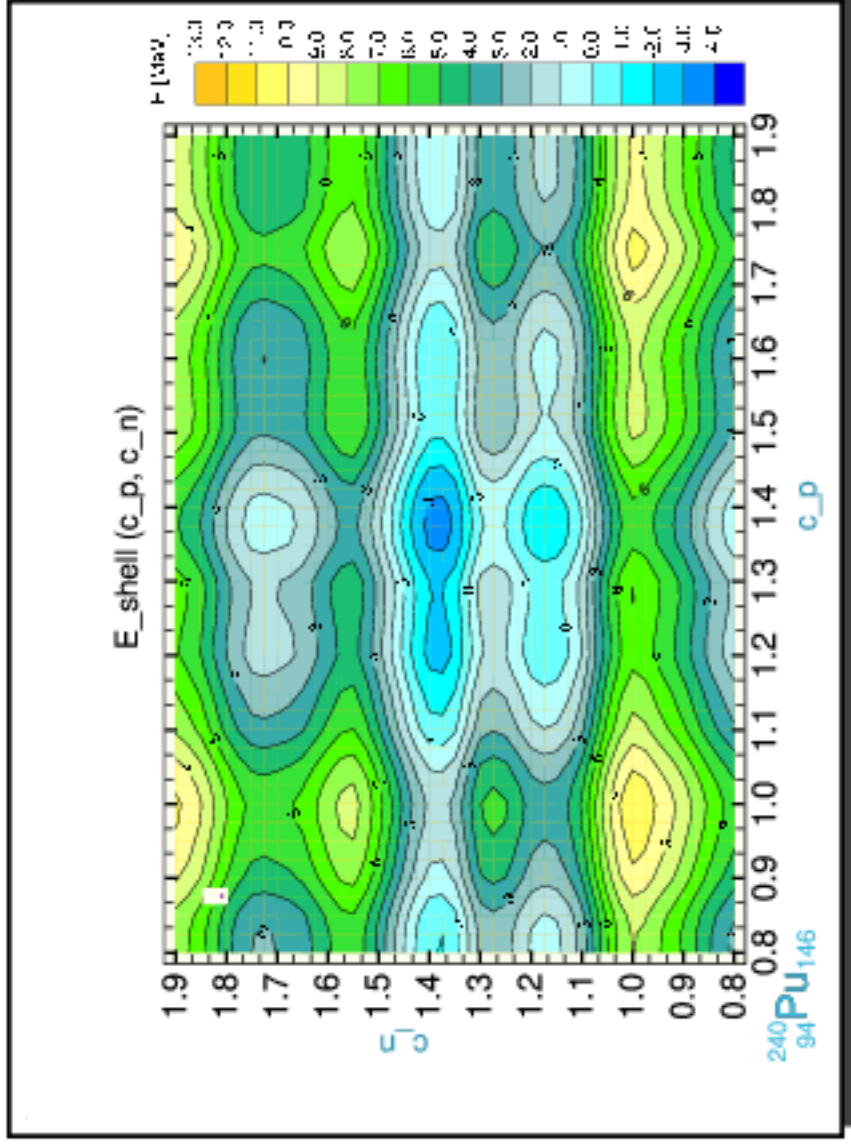
Stiffness of E_{mac} against different p-n deformations



Variation of macroscopic Yukawa-folded energy for ^{234}Th as function of the proton \leftrightarrow neutron deformation difference

Shell + pairing effects

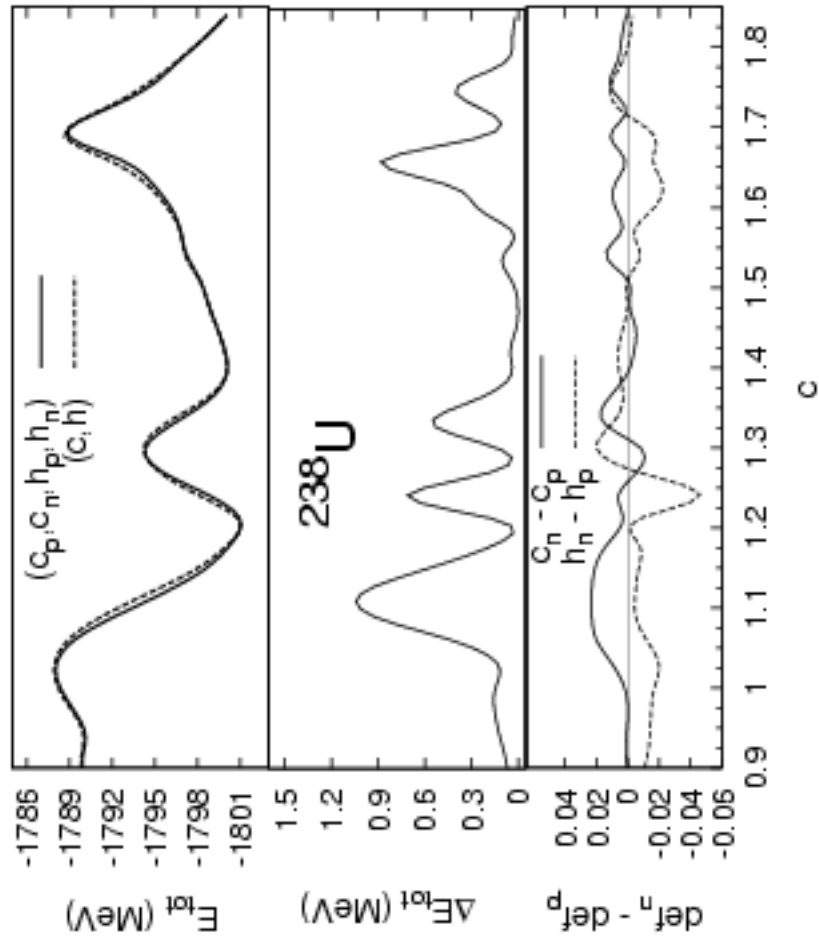
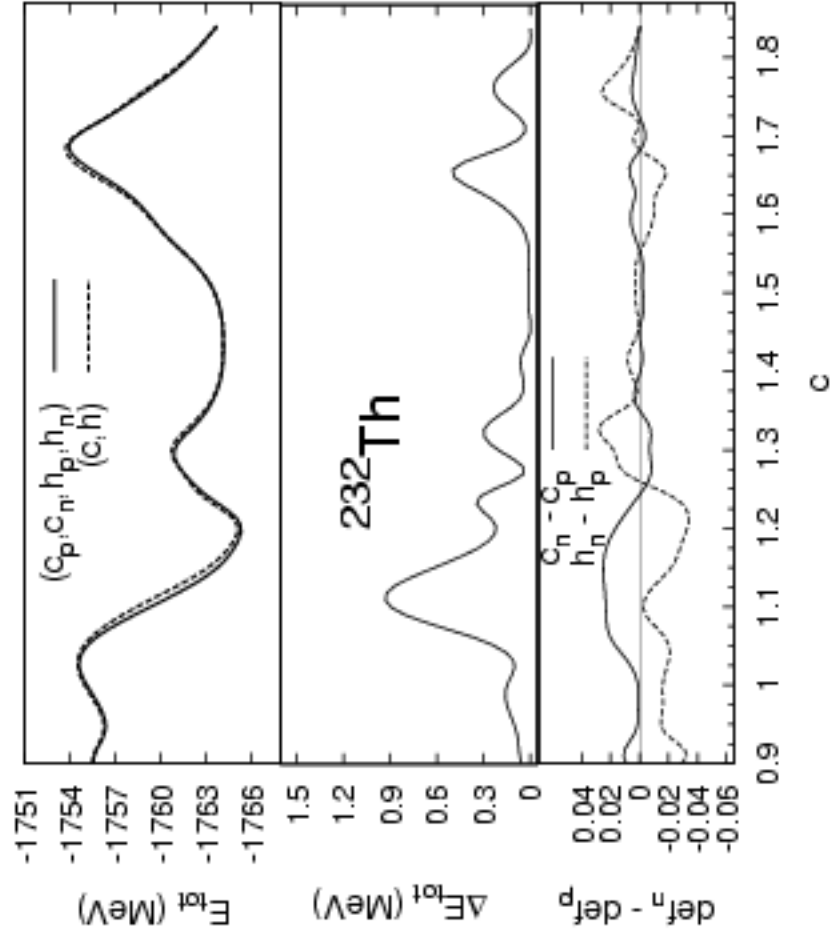
can favour such deformation difference

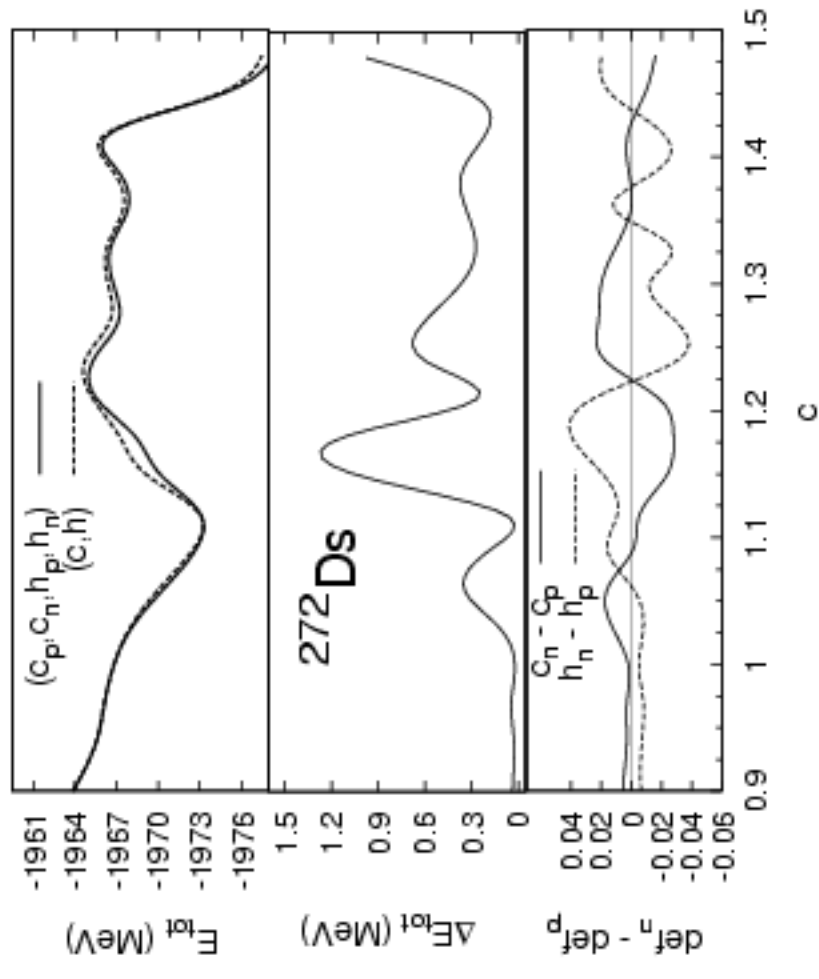
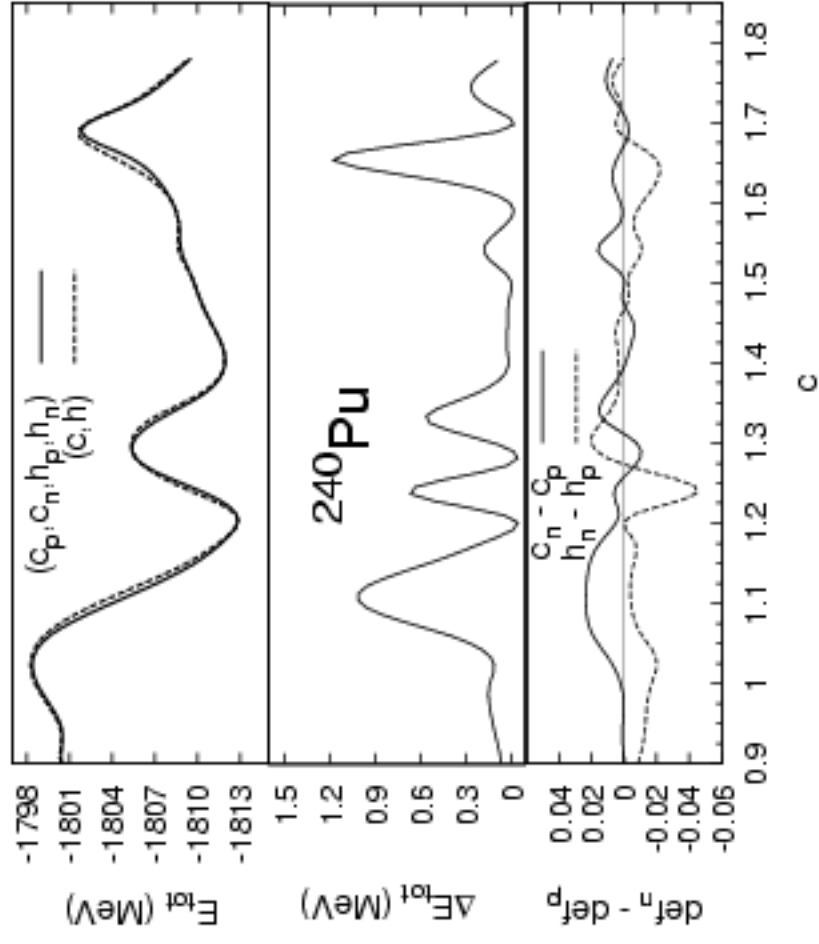


$$E_{tot} = E_{\text{mac}}(\text{def}_p, \text{def}_n) + \delta E_{\text{mic}}(\text{def}_p, \text{def}_n)$$

$$E_{\text{mac}}(\text{def}_p, \text{def}_n) = E_{\text{LSD}}(\text{def}) + E_{\text{pot}}(\text{def}_p, \text{def}_n) - E_{\text{pot}}(\text{def}, \text{def})$$

$$\delta E_{\text{mic}} = \delta E_{\text{shell}} + \delta E_{\text{pair}}$$





Barriers with left-right asymmetric and non-axial shapes

Use now full 4-D $\{c, h, \alpha, \eta\}$ deformation space

- generally admitted:
- non axial 1st barrier
 - left-right asymmetric 2nd barrier

BUT

- strong variation of shell effects from one nucleus to the next
- strong variation of energy landscape on the way to scission
 \implies location of saddle points is difficult

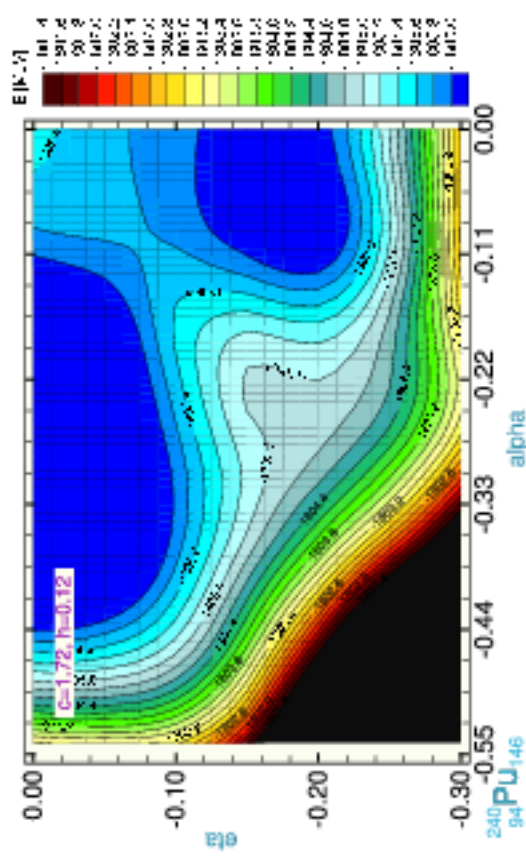
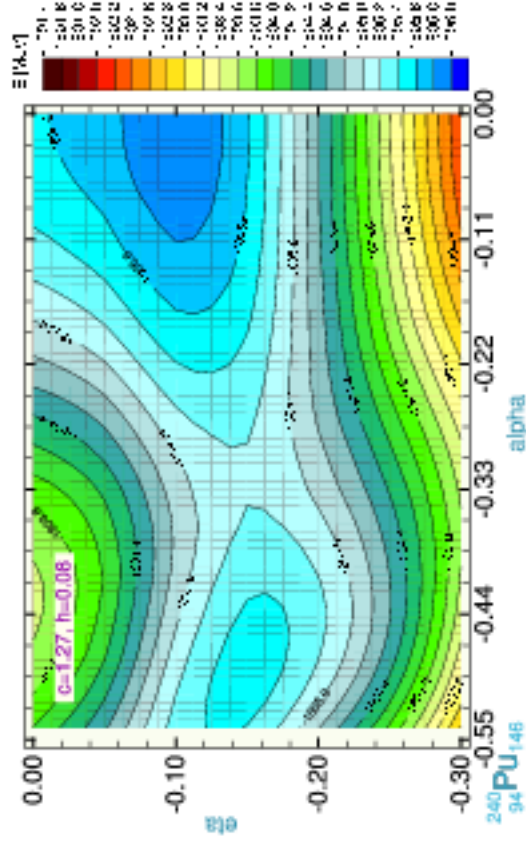
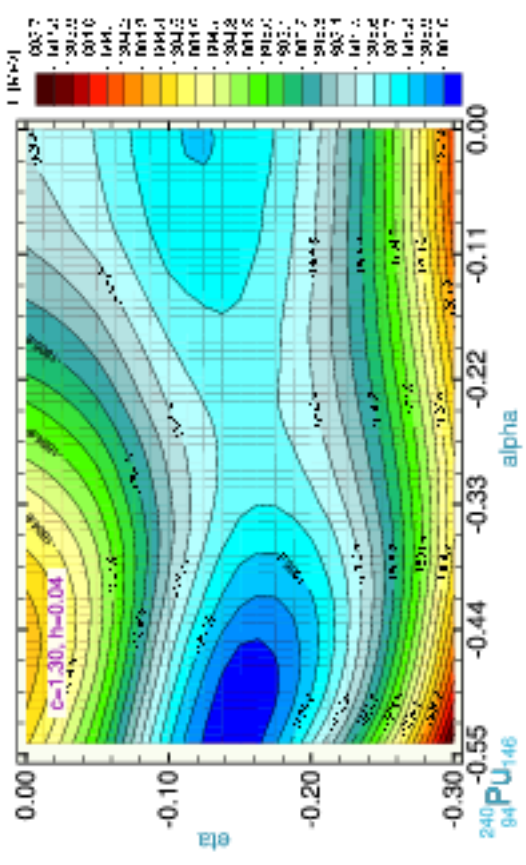
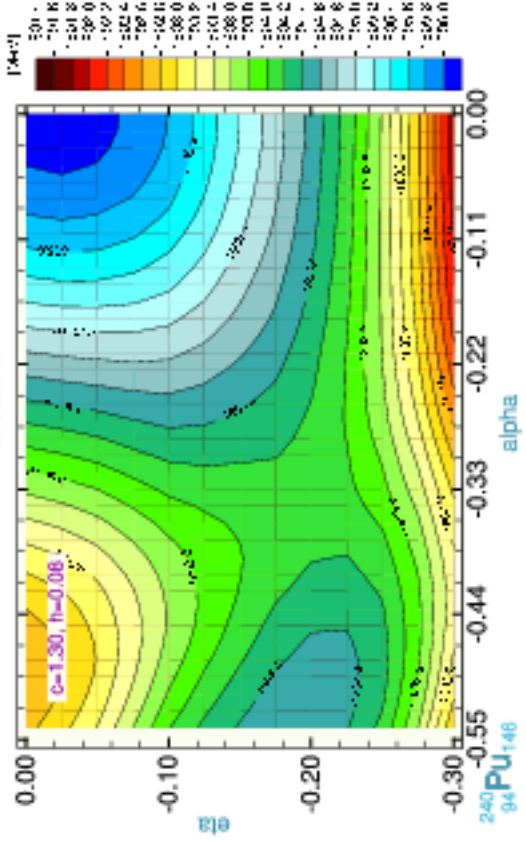
use gradient method

$$|\vec{\nabla} V_{pot}| = \sqrt{\left(\frac{\partial V_{pot}}{\partial c}\right)^2 + \left(\frac{\partial V_{pot}}{\partial h}\right)^2 + \left(\frac{\partial V_{pot}}{\partial \alpha}\right)^2 + \left(\frac{\partial V_{pot}}{\partial \eta}\right)^2} = 0$$

diagonalize the matrix $\frac{\partial^2 V_{pot}}{\partial \alpha_i \partial \alpha_j}$

decide whether maximum, minimum or saddle point

first saddle



Nucleus	Ground state		Inner saddle point				Outer saddle point				
	Mass (MeV)		α	η	ΔE	B_f^{th}	α	η	ΔE	B_f^{th}	
232Th	-1765.3	0.8	0.06	0.10	0.4	5.0	0.42	0.05	5.5	4.5	-0.9
234Th	-1776.5	0.5	0.03	0.10	0.3	5.2	0.39	0.05	6.6	4.4	-1.4
234U	-1777.1	0.8	0.12	0.0	0.4	4.4	0.30	0.0	4.9	3.8	-1.1
236U	-1789.3	0.4	0.06	0.0	0.2	5.5	0.33	0.0	6.3	3.5	-1.7
238U	-1800.8	0.2	0.0	0.05	0.1	6.7	0.33	0.05	6.9	4.2	-1.4
240U	-1811.8	-0.1	0.06	0.10	0.3	6.5	0.33	0.0	7.2	3.8	-2.1
236Pu	-1787.2	0.5	0.15	0.05	0.2	5.9	0.33	0.0	4.3	3.6	-0.4
238Pu	-1800.3	0.2	0.09	0.0	0.1	6.5	0.36	0.0	4.2	4.5	-0.4
240Pu	-1812.7	0.0	0.06	0.10	0.4	7.0	0.21	0.0	6.1	3.7	-1.6
242Pu	-1824.5	-0.2	0.09	0.10	0.5	7.1	0.30	0.0	6.3	4.2	-1.3
244Pu	-1835.6	-0.3	0.09	0.10	0.8	6.9	0.33	0.05	4.9	5.2	-0.3
246Pu	-1846.8	-0.9	0.03	0.15	1.1	7.2	0.30	0.05	5.0	4.5	-1.7
242Cm	-1822.7	-0.1	0.09	0.20	0.7	7.1	0.24	0.0	5.2	3.4	-0.7
244Cm	-1835.3	-0.2	0.06	0.10	0.9	7.2	0.27	0.05	5.1	4.2	-0.3
246Cm	-1847.1	0.0	0.06	0.15	1.4	6.8	0.21	0.05	4.7	4.5	-0.2
248Cm	-1858.4	0.0	0.06	0.15	1.8	6.6	0.21	0.10	3.2	5.2	0.2
250Cm	-1868.8	0.2	0.12	0.10	1.1	5.9	0.27	0.05	3.5	4.3	0.1
250Cf	-1869.0	0.2	0.09	0.15	2.2	6.5	0.06	0.05	3.6	3.8	0.2

What can we conclude?

- ground-state masses very well reproduced (~ 0.5 MeV)
- saddle-point masses \sim OK (slightly too high ~ 0.8 MeV)
 - But that is good news
 - ▷ Deformation dependence of *Congruence* energy ~ 0.1 MeV
 - ▷ Additional degrees of freedom like proton-neutron deformation difference
 - ▷ Shape dependence of average pairing energy
- masses of 2nd saddle seem to high

But: exp. masses of 2nd saddle *very* model dependent

Conclusions

- Fission barriers very well described by the macroscopic-microscopic YF + LSD approach
- different proton-neutron deformations can change fission barriers *locally* by ~ 1 MeV
- left-right asymmetric shapes also present at the 1st barrier
- non axial shapes also present at the 2nd barrier
- same kind of description for super-heavy nuclei (**under way**)
- include 4-D shape description in Langevin approach